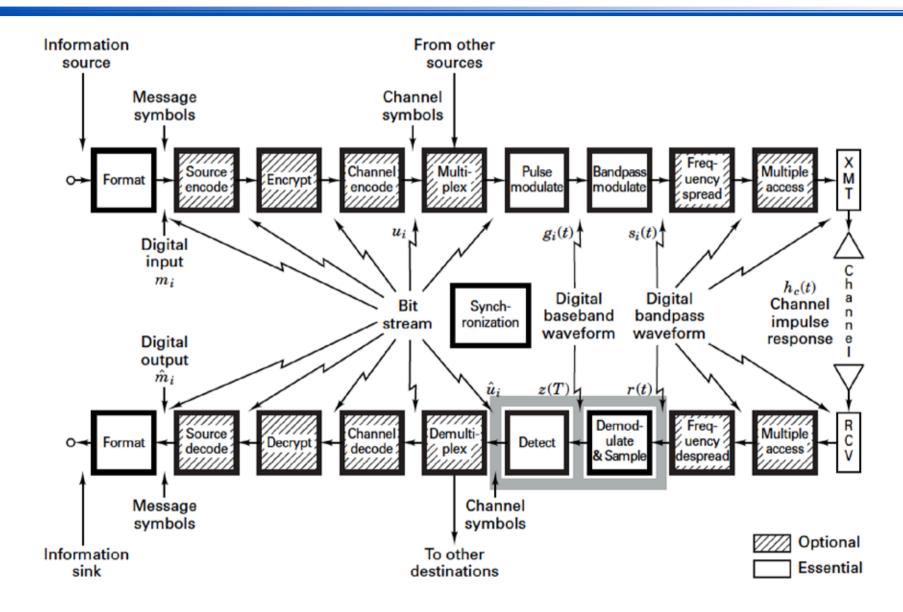
#### **CSE4214 Digital Communications**

### **Chapter 3 Part 2**

#### **Baseband Demodulation/ Detection**

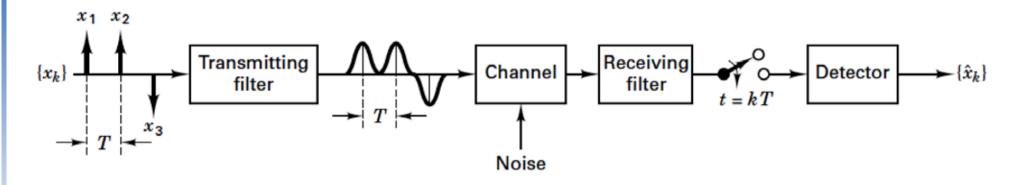
#### **Baseband Demodulation/Detection**



#### **CSE4214 Digital Communications**

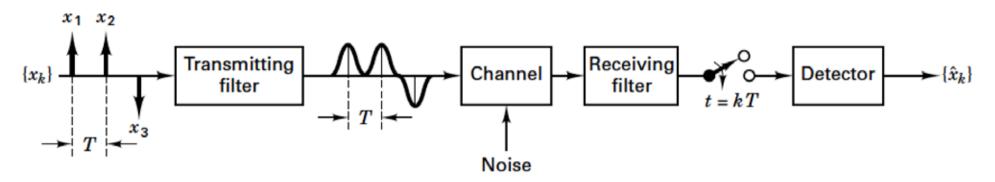
#### **Intersymbol Interference**

#### Filtering Aspect of a Digital Communication System



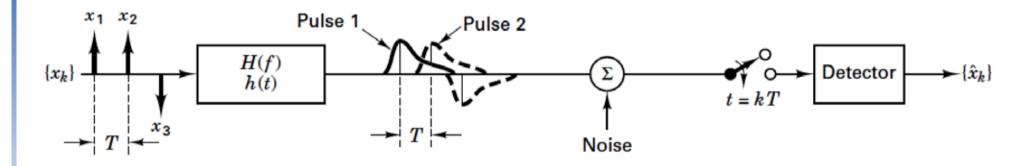
- There are various filters throughout the system: at transmitter, at receiver, and at channel.
  - At the transmitter: transmitting filter  $H_t(f)$
  - At the channel, distributed reactances for cable or fading channel for wireless. We use  $H_c(f)$  to represent the filtering effect.
  - At the receiver: receiving filter  $H_r(f)$

## **Functions of Filters**



- 1. <u>Transmitting filter  $H_t(f)$ </u>: The input to the transmitting filter are impulses denoting the information symbols  $\{x_k\}$ . Bit 1 is represented by a positive impulse and bit 0 by a negative impulse. These impulses modulate rectangular pulses such that bit 1 is now represented by a positive rectangular pulse and bit 0 by a negative rectangular pulse. Since the bandwidth of a rectangular pulse is infinite, the rectangular pulses are band limited by the transmitting filter.
- 2. <u>Channel  $H_c(f)$ </u>: The channel is modeled by a LTI system with a transfer function  $H_c(f)$ . It accounts for distortion produced, for example, by fading or by bandwidth constraints.
- 3. <u>Receiving filter  $H_r(f)$ </u>: The receiving filter compensates for distortion resulting from the transmitter and the channel. It models both the receiving and equalizing filters. 5

# An Equivalent Model

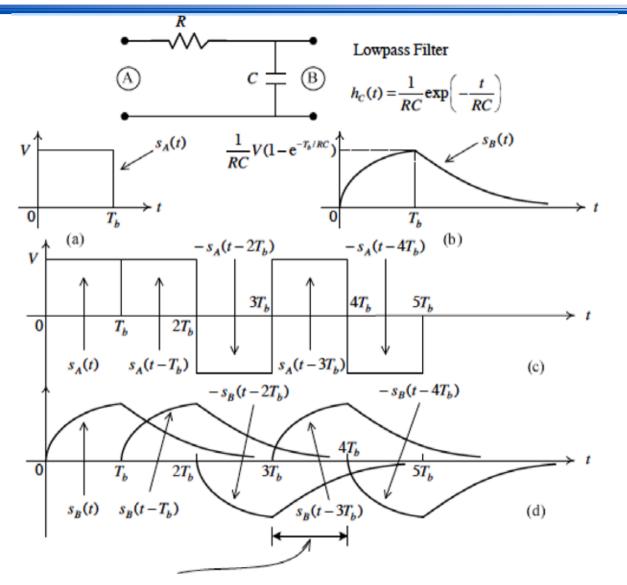


- Lumping all the filtering effects into one overall equivalent system transfer function:  $H(f) = H_t(f) H_c(f) H_r(f)$ .
- The pulses at the output of the equivalent filter overlap each other.
   This effect is called **intersymbol interference** (ISI).
- ISI restricts the transmission rate of a communications system. Clearly if the transmission rate  $R_s$  is increased (*T* is reduced), then the ISI will also increase.

# Intersymbol Interference (ISI)

- A form of distortion of a signal in which one symbol interferes with subsequent symbols.
- Mainly caused by multipath propagation (in wireless) or the inherent non-linear response of a channel.
- ISI causes successive symbols to "blur" together.
- ISI occurs even in the absence of noise (due to the effects of filtering and channel-induced distortions)

### **ISI Example**



In this interval:  $y(t) = b_0 s_B(t) + b_1 s_B(t-T) + b_2 s_B(t-2T) + b_3 s_B(t-3T) + n_0(t)$ 

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### **Nyquist Criterion for Zero ISI**

$$y(t) = \sum_{k=-\infty}^{\infty} b_k s_R(t - kT) + n_0(t)$$

where  $s_R(t) = h_T(t) * h_C(t) * h_R(t)$  is the overall response of the system due to a unit impulse at the input

$$b_{k} = \begin{cases} V & \text{if the } k^{th} \text{ bit is } 1\\ -V & \text{if the } k^{th} \text{ bit is } 0 \end{cases}$$

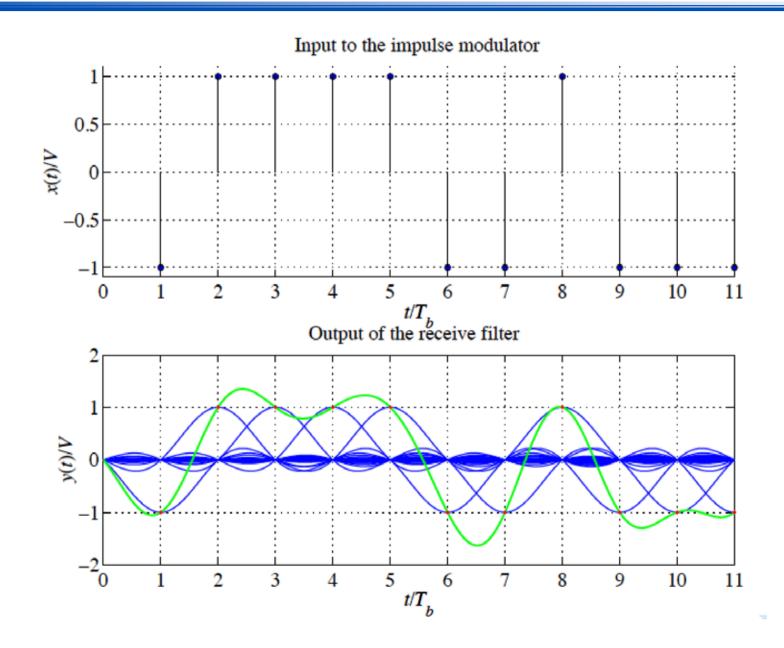
Normalize  $s_R(0)=1$ , and take at sampling time t=mT

$$y(mT) = b_m + \sum_{\substack{k=-\infty\\k\neq m}}^{\infty} b_k s_R(mT - kT) + n_0(mT)$$
ISI term



# Under what conditions the Nyquist Criterion for zero ISI holds?

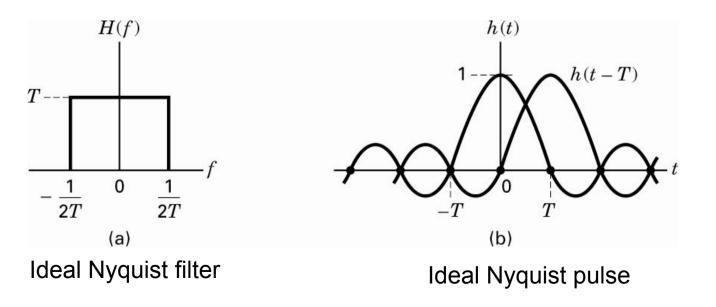
### Zero ISI Example



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#### Nyquist Theoretical Minimum System Bandwidth

- The theoretical minimum bandwidth needed in order to detect  $R_s$  symbols/s, without ISI, is  $R_s/2$  Hz.
- This occurs when the system transfer function is made rectangular.
- For baseband systems, the rectangular bandwidth is called ideal Nyquist filter.
- The sinc(t/T)-shaped pulse is called ideal Nyquist pulse.

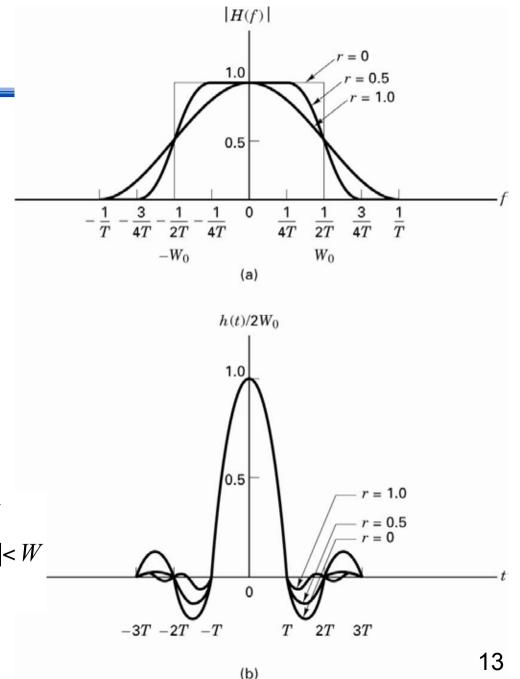


#### **Raised Cosine Filter (1)**

- A system having the overall transfer function *H*(*f*) as a rectangular pulse is difficult to be implemented:
- 1. The overall amplitude transfer function H(f)has to be flat over the range -1/2T < f < 1/2Tand zero outside the range. This is physically unrealizable because the impulse response is infinitely long and non-causal.
- 2. The synchronization of the clock in the detector has to be perfect at instants t = kT.
- An alternative transfer function is the raisedcosine transfer function

$$H(f) = \begin{cases} 1 & \text{for } |f| < 2W_0 - W \\ \cos^2 \left[ \frac{\pi}{4} \frac{|f| + W - 2W_0}{W - W_0} \right] & \text{for } 2W_0 - W < |f| < W \\ 0 & \text{for } |f| > W \end{cases}$$

where roll-off factor  $r = (W - W_0)/W_0$ 



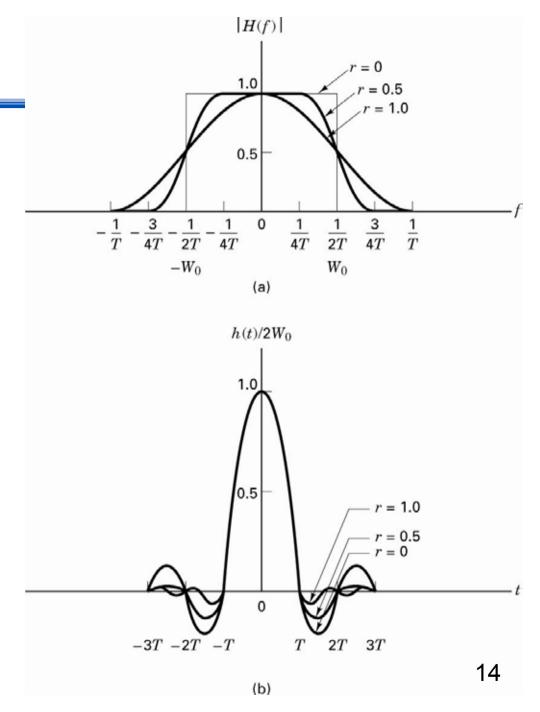
#### **Raised Cosine Filter (2)**

• The impulse response of the raised cosine filter is given by

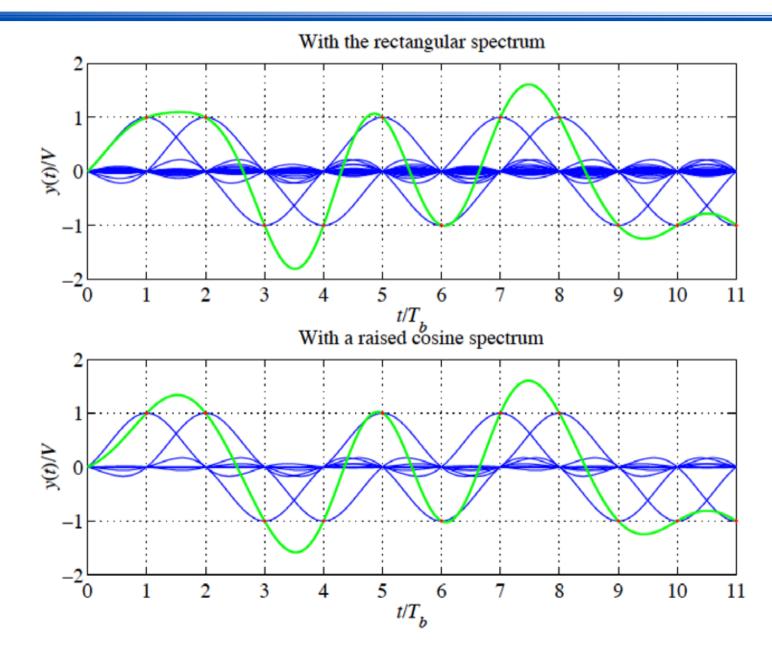
$$h(t) = 2W\left(\operatorname{sinc}(2W_0 t)\right) \frac{\cos[2\pi (W - W_0)t]}{1 - [4(W - W_0)t]^2}$$

• The minimum system bandwidth required for a symbol rate of *R<sub>s</sub>* with the raised cosine filter is given by

$$W = \frac{1}{2}(1+r)R_s$$



#### Zero ISI - Raised Cosine Example



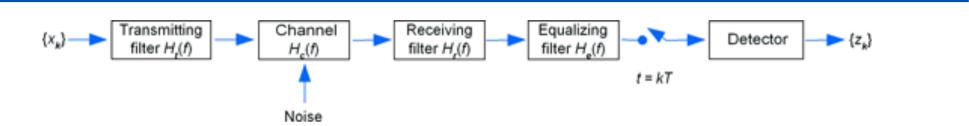


Find the minimum required bandwidth for the baseband transmission of a 4-level PAM pulse sequence having a date rate of R = 2400 bit/s if the system transmission characteristic consist of a raised cosine spectrum with 100% excess bandwidth (r = 1).

#### **CSE4214 Digital Communications**

#### **Equalization**

### **Channel Characterization**



— The baseband digital communication system is modified such that the equalizing and receiving filters are considered as separate blocks.



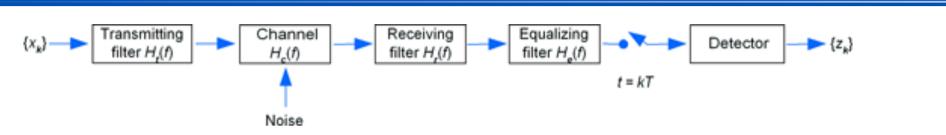
The equivalent transfer function is obtained by lumping all of the transfer functions in one system as

$$H(f) = H_t(f)H_c(f)H_r(f)H_e(f).$$

 In practice, the transmitting and receiving filters are chosen so that the product is equal to the Nyquist raised cosine transfer function. For example,

 $H_t(f)H_r(f)=H_{\rm \tiny RC}(f).$ 

# Equalization



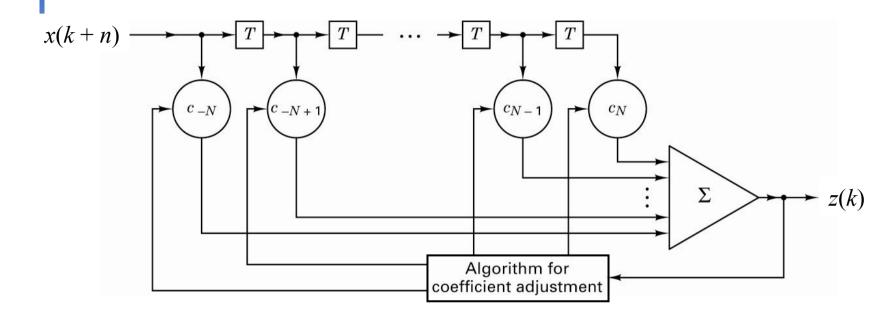
 The equalizing filter attempts to eliminate any distortion produced by the channel. If we model the channel as

$$H_c(f) = |H_c(f)| \ e^{j\theta_c(f)}$$

where  $|H_c(f)|$  represents the magnitude and  $\theta_c(f)$  represents the phase. To compensate for the channel distortion, the equalizing filter is implemented such as

$$H_{e}(f) = \frac{1}{H_{c}(f)} = \frac{1}{|H_{c}(f)|} e^{-j\theta_{c}(f)}$$

#### **Equalizer Filter – Transversal Equalizer**

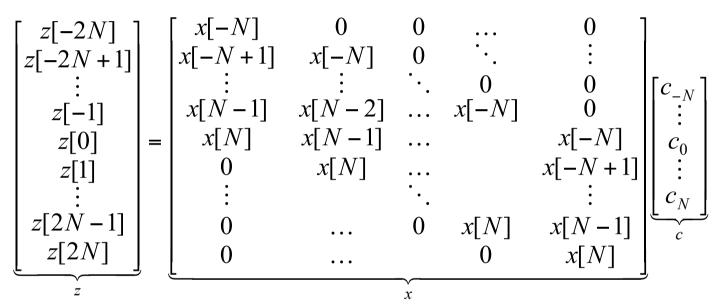


- The transversal filter shown above is commonly used for equalization.
- The output of the transversal filter is given by convolving the input samples and tap weights:

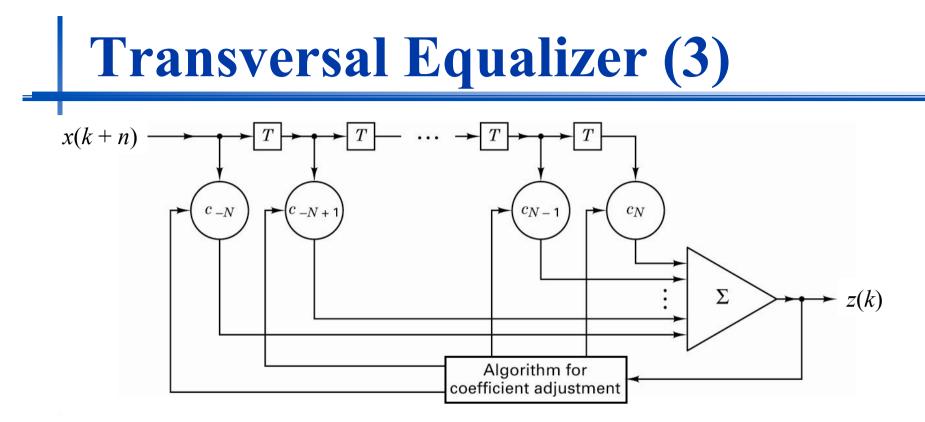
$$z[k] = \sum_{n=-N}^{N} x[k-n]c_n$$
 for  $k = -2N,...,2N$  and  $n = -N,...,N$ 

### **Transversal Equalizer (2)**

• The convolution can be expressed as:



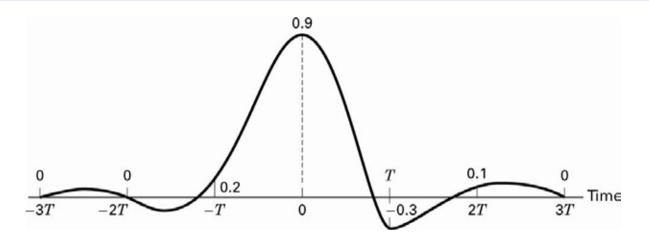
- Or a more compact form as: **z**=**xc**
- Solving  $c = x^{-1}z$  is possible only if x is a square matrix.
- Note: the size of the vector **z** and the number of rows in the matrix **x** may be chosen to be any value. It depends on the number of ISI points interested



- Solving  $c = x^{-1}z$  is possible only if x is a square matrix.
- Alternatively, the zero-forcing solution is obtained by disposing the top N and bottom N rows of the matrix x and vector z.
- To avoid ISI, the value of z is assumed to be

$$z[k] = \begin{cases} 1 & k = 0 \\ 0 & k = \pm 1, \dots, \pm N \end{cases}$$





- 1. A single impulse is transmitted through a digital communication system with the above waveform received, i.e. [x(k)]=[0.0, 0.0, 0.2, 0.9, -0.3, 0.1, 0.0]. Use a zero-forcing solution to find the weights  $\{c_k\}$  (*k*=-1,0.1) of a 3-tap transversal equalizer that reduce the ISI so that the equalized pulse samples z(k) have the values [z(-1)=0, z(0)=1, z(1)=0].
- 2. Using the weights obtained in (1), determine the ISI values of the equalized pulse at sample times  $k = \pm 1, \pm 2, \text{ and } \pm 3$ .
- 3. What is the largest magnitude sample contributing to the ISI and what is the sum of all of the ISI magnitudes?

# **Measuring ISI - Eye Pattern**

- Eye patterns are obtained by applying the communication system's response to the vertical plates of an oscilloscope.
- A sawtooth wave with fundamental frequency equal to the symbol rate is applied to the horizontal plates of the oscilloscope.
- The setup superimposes the communication system's response within each signaling interval on top of each other within a single interval (0,*T*).
- The maximum eye opening  $(M_N)$  provides a good estimate of the optimal sampling instant.
- The width  $(S_T)$  of the eye opening is the range over which the sampling may be performed.
- The range  $(D_A)$  of the amplitude variations provide an estimate of the ISI.
- The range  $(J_T)$  of the time differences of the zero crossings provide an estimate of jitter.

