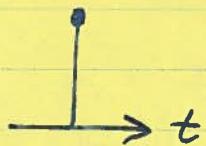
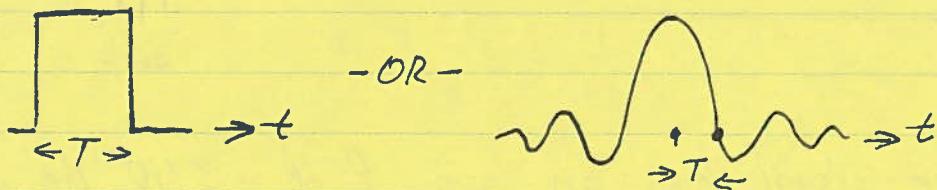


L14 Bandpass Modulation

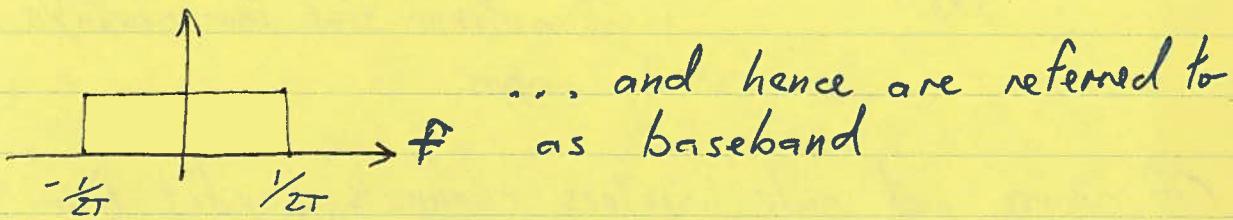
14.1 Basics

- So far we have represented ~~our~~ our digital messages as impulses...

 ... of discrete amplitudes that are represented as analog waveforms (symbols)...



... with spectra that encompass DC...



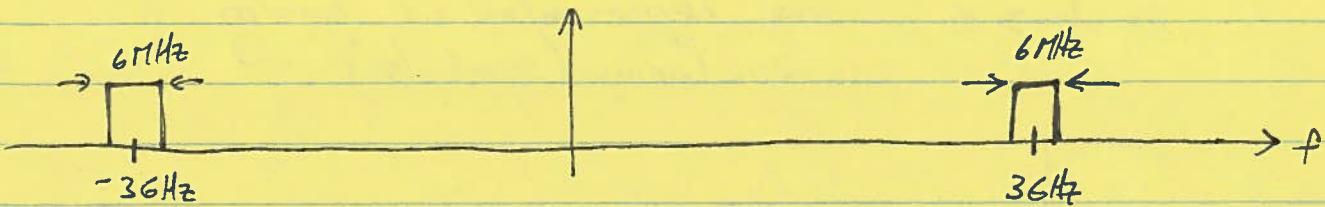
- Unfortunately many physical channels have trouble with such low frequencies
- A prominent example is wireless which require antennas whose size (length) is $\sim \lambda$ (avg. wavelength of the signal being transmitted/received)

$$\dots \text{but recall } \lambda = \frac{c}{f}$$

- So if you want to send a 10Mbps signal that fits within a bandwidth of say 3MHz

$$\lambda = \frac{3 \times 10^8}{3 \times 10^6} = 100\text{m} \leftarrow \text{the size of an efficient antenna}$$

- In this case you'd rather send



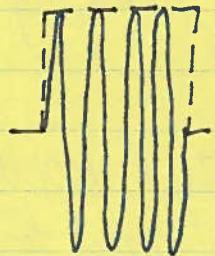
- now your signal has an avg. f of $3 \times 10^9 \text{ Hz}$

$$\lambda = \frac{3 \times 10^8}{3 \times 10^9} = 10\text{cm} \dots \text{a much more manageable antenna size for portable apps.}$$

- Of course not only wireless channels benefit from such bandpass signalling
- The ability to shift your signal in frequency sets up opportunities for advanced modulation schemes that not only allow you to send signals better matched to the characteristics of your channel, but to share that channel among multiple users very efficiently (channelization)
- For example, ADSL uses a sophisticated bandpass modulation scheme to get high bandwidth internet over telephone lines

14.2 Bandpass Signalling

- Instead of just pulses you are sending modulated sine waves



- on -



- In general you have ...

$$s(t) = A(t) \cos[\omega_0 t + \phi(t)]$$

... and therefore 3 parameters which can be used to represent data

amplitude : $A(t)$

frequency : ω_0
phase : $\phi(t)$

Note: $A_{rms} = \sqrt{\frac{1}{T} \int_0^T (A \cos(\omega t))^2 dt} = \frac{A}{\sqrt{2}}$

$$\therefore A = \sqrt{2} A_{rms} = \sqrt{2 A_{rms}^2} = \sqrt{2 P_{avg. power}} = \sqrt{\frac{2 E}{T}}$$

- common to designate carrier amplitude in terms of signal energy per symbol

(4)

- the high freq. waveform that you are modulating is generally referred to as the carrier
- broadly speaking there are 2 methods of handling (demodulating) passband waveforms

COHERENT DEMODULATION

- RX has to figure out the phase of the carrier (even if that's not the part that your data has modulated)

- more complex
- better P_b

- some bandpass modulation examples

NONCOHERENT DEMODULATION

- RX does not need to figure out phase of carrier

- less complex
- worse P_b

14.3 PSK: Phase Shift Keying

$$s_i(t) = \sqrt{\frac{2E}{T}} \cos[\omega_0 t + \phi_i(t)] \quad 0 \leq t \leq T \\ i = 1, \dots, M$$

$$\phi_i(t) = \frac{2\pi i}{M}$$

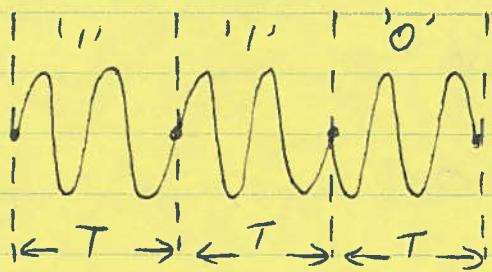
'1' '0'

e.g. in the binary case, $M=2$: $\phi_1(t)=0$ $\phi_2(t)=\pi$
 (or vice-versa)

BPSK

(5)

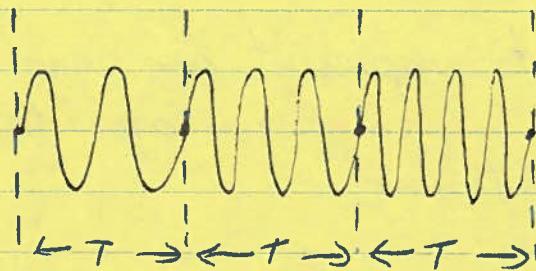
and in time the signal looks like



14.4 FSK: Frequency Shift Keying

$$s_i(t) = \sqrt{\frac{2E}{T}} \cos(\omega_i t + \phi) \quad 0 \leq t \leq T$$

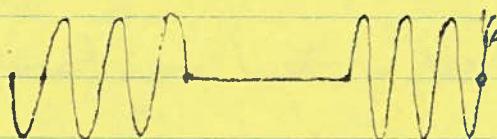
ω_i has M discrete values



14.5 ASK: Amplitude Shift Keying

$$s_i(t) = \sqrt{\frac{2E_i(t)}{T}} \cos(\omega_0 t + \phi)$$

- simple 2-level case: ON-OFF KEYING (OOK)



(6)

14.6 APK: Amplitude Phase Keying

- A combination of ASK + PSK

$$s_i(t) = \sqrt{\frac{2E_i(t)}{T}} \cos(\omega_0 t + \phi_i(t))$$

- e.g. m-ary QAM

14.7 Signal Space Concepts

- A powerful way to view our symbol waveforms follows a geometric perspective
- In particular, it is possible to represent our signal by an orthonormal function series expansion analogous to classical Fourier series representation
- These functions effectively define the coordinates of some multidimensional space and hence allow us to view our signal (symbol) as some vector in this multidimensional space
- Formally we refer to these coordinate defining functions as basis functions

$$\psi_m(t) \quad m=0,1,\dots \quad (\text{set of real waveforms})$$

- defined over some interval $T_i \rightarrow T_f$

initial \rightarrow \leftarrow final

(7)

- Number of functions and their interval does not have to be finite
- the functions that define the coordinates of our space must be perpendicular to each other... **ORTHONORMAL**

$$\int_{T_i}^{T_f} \psi_i(t) \psi_j(t) dt = \delta_{ij} = \begin{cases} 1 & \text{if } i=j \\ 0 & \text{if } i \neq j \end{cases}$$

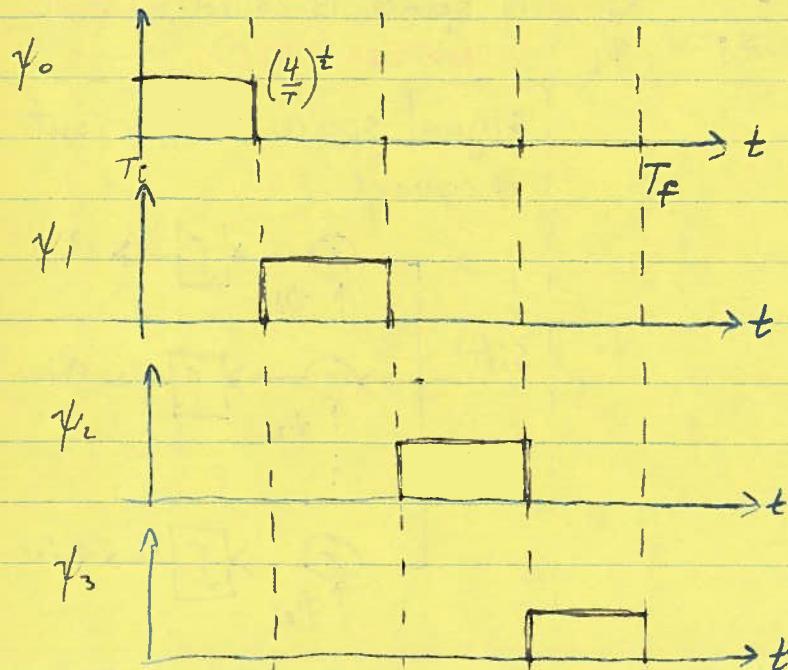
Kronecker delta function

(basis fns. look like they are unit energy)

- e.g. in the case of a fn. described by a Fourier Series (F.S.) the F.S. coefficients define an infinite dimensional space over $T = T_f - T_i$ where $T = \frac{2\pi}{\omega_0}$ and...

$$\dots \psi_m(t) = \left\{ \left(\frac{1}{T}\right)^{\frac{1}{2}}, \left(\frac{2}{T}\right)^{\frac{1}{2}} \cos(m\omega_0 t), \left(\frac{2}{T}\right)^{\frac{1}{2}} \sin(m\omega_0 t), \dots \right\} m=1, 2, \dots$$

- another example is the finite set of N nonoverlapping pulses



- suppose a class of deterministic signals $s_i(t) \ i=1, 2, \dots M$ (an M -ary set) each has a finite energy
- we can (it can be shown) express these as an N -term series expansion of **orthonormal basis functions**

$$s_i(t) = \sum_{j=1}^N a_{ij} \psi_j(t)$$

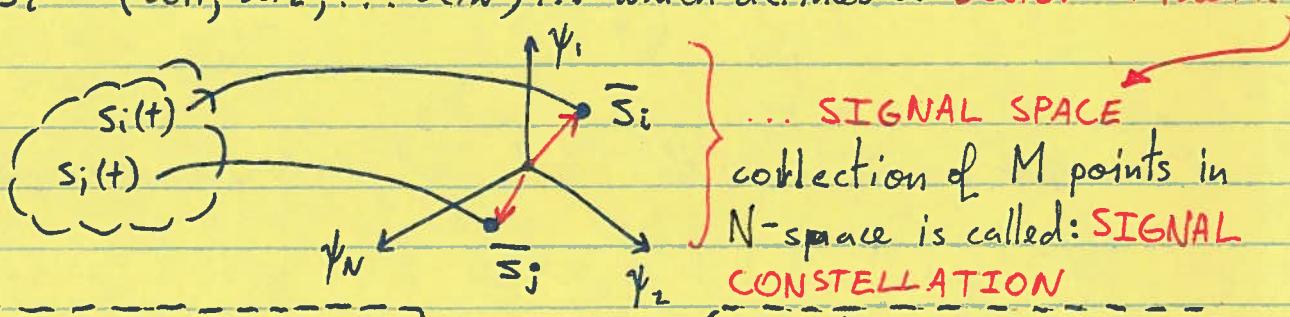
- where the **expansion coefficients**, a_{ij} , are found with

$$a_{ij} = \int_{T_1}^{T_p} s_i(t) \psi_j(t) dt$$

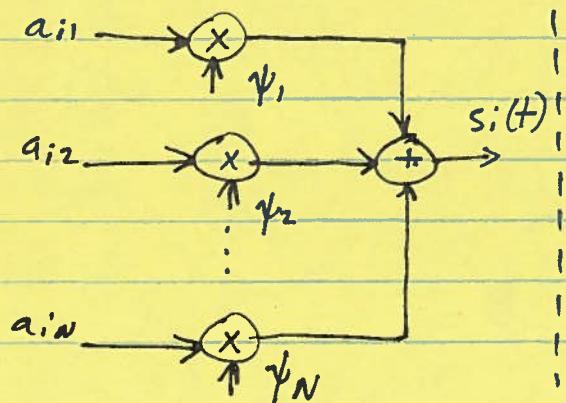
basis fn.

} **INTERPRET** as projection of i th symbol on j th basis function

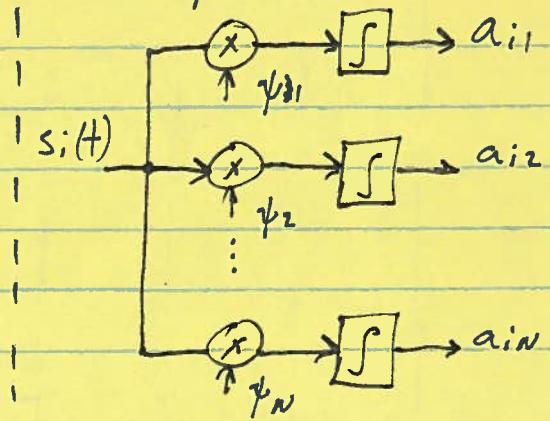
- thus every symbol $s_i(t)$ of M -ary set is mapped onto some N -dimensional space at coordinate $\bar{s}_i = (a_{i1}, a_{i2}, \dots, a_{iN})$... which defines a **vector** in the...



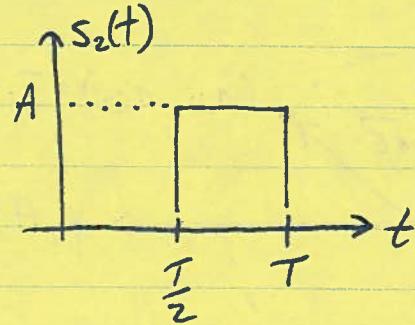
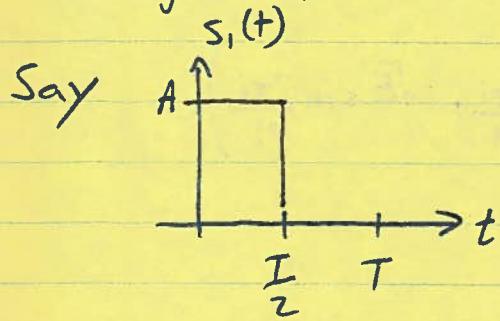
signal generation from
signal space coefficients



signal space coefficient
recovery

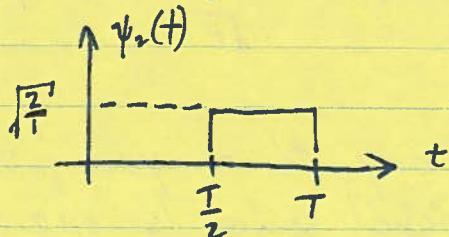
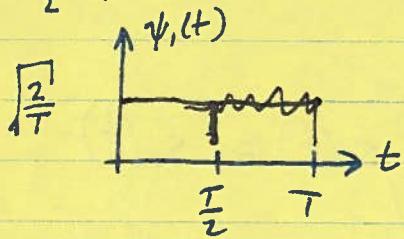


14.8 Signal Space Examples



- the original symbols are already orthogonal
- just need to scale these to make orthonormal basis functions

$$\left(\frac{T}{2} \cdot y^2 = 1 \Rightarrow y = \sqrt{2/T}\right)$$



- two-dimensional signal-space representation

$$\begin{aligned} \psi_2 \otimes \psi_1 &\uparrow \frac{A}{\sqrt{2}} = \bar{s}_2 \\ &\downarrow \frac{A}{\sqrt{2}} = \bar{s}_1 \end{aligned}$$

$\alpha \otimes \beta_1$

try M-ary PSK...

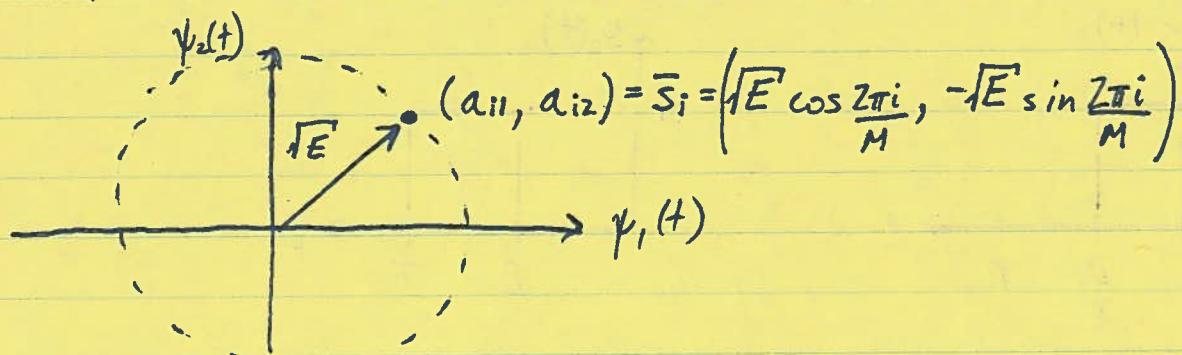
$$s_i(t) = \sqrt{\frac{2E}{T}} \cos\left(\omega_0 t + \frac{2\pi i}{M}\right) \quad i=0, 1, \dots, M-1$$

$$0 \leq t \leq T$$

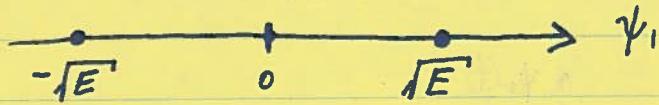
by trig identities obvious that

$$\psi_1(t) = \sqrt{\frac{2}{T}} \cos \omega_0 t \quad \psi_2(t) = \sqrt{\frac{2}{T}} \sin \omega_0 t$$

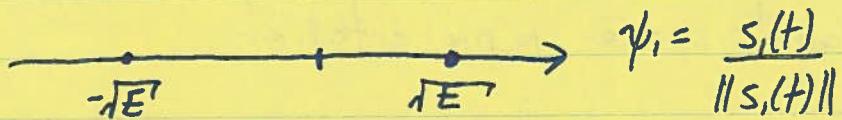
so M-PSK sets have 2-dim. constellations



For 2-PSK = BPSK ... we only have a 1-dimensional constellation



- in general any time you just have $s_1(t) = -s_2(t)$
- then your signal space is one dimensional



QAM ... a popular modulation technique with a 2-dimensional signal space

$$s_i(t) = a_i \sqrt{\frac{2}{T}} \cos \omega t + b_i \sqrt{\frac{2}{T}} \sin \omega t \quad 0 \leq t \leq T \quad i=0, 1, \dots, M-1$$

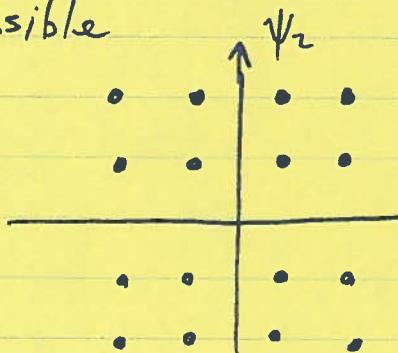
our standard PSK basis functions

if all signals have equal energy : $(a_i^2 + b_i^2)^{\frac{1}{2}} = E^{\frac{1}{2}}$

modulation is strictly through phase and QAM is just M-PSK

- otherwise with QAM all manner of 2-D constellation arrangements are possible

$M = 16$



← such rectangular constellation arrangements are very common

- a common variation is pulse shaped QAM

$$s_i(t) = h_T(t) [a_i \cos \omega_0 t + b_i \sin \omega_0 t] \quad -\infty < t < \infty \quad i=0, 1, \dots, M-1$$

↑
tx filter response

- basis set is modified by h_T ... but 2D signal constellation is unchanged

